



Inverse problems for the transient eddy current equation

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Motivation

Inverse Electromagnetics & Eddy currents



Inverse Electromagnetics

Inverse Electromagnetics:

- Generate EM field (drive excitation current through coil)
- Measure EM field (induced voltages in meas. coil)
- Gain information from measurements

Applications:

- Metal detection (buried conductor)
- Non-destructive testing (crack in metal, metal in concrete)





Maxwell's equations

Classical Electromagnetics: Maxwell's equations

 $\begin{aligned} \operatorname{curl} H &= \epsilon \partial_t E + \sigma E + J & \text{in } \mathbb{R}^3 \times]0, T[\\ \operatorname{curl} E &= -\mu \partial_t H & \text{in } \mathbb{R}^3 \times]0, T[\end{aligned}$

E(x, t):Electric field $\epsilon(x)$:PermittivityH(x, t):Magnetic field $\mu(x)$:PermeabilityJ(x, t):Excitation current $\sigma(x)$:Conductivity

Knowing $J, \sigma, \mu, \epsilon + init.$ cond. determines E and H.



Eddy currents

Maxwell's equations

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$$\begin{aligned} \operatorname{curl} H &= \epsilon \partial_t E + \sigma E + J & \text{in } \mathbb{R}^3 \times]0, T[\\ \operatorname{curl} E &= -\mu \partial_t H & \text{in } \mathbb{R}^3 \times]0, T[\end{aligned}$$

Eddy current approximation: Neglect displacement currents $\epsilon \partial_t E$

 Justified for low-frequency excitations (Alonso 1999, Ammari/Buffa/Nédélec 2000)

$$\partial_t(\sigma E) + \operatorname{curl}\left(rac{1}{\mu}\operatorname{curl} E
ight) = -\partial_t J \quad ext{in } \mathbb{R}^3 imes]0, \, \mathcal{T}[$$



Where's Eddy?

• $\sigma = 0$: (Quasi-)Magnetostatics

$$\operatorname{curl}\left(rac{1}{\mu}\operatorname{curl} E
ight) = -\partial_t J$$

Excitation $\partial_t J$ instantly generates magn. field $\frac{1}{\mu} \operatorname{curl} E = -\partial_t H$.

• $\sigma \neq 0$: Eddy currents

$$\partial_t(\sigma E) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E\right) = -\partial_t J$$

 $\partial_t J$ generates changing magn. field + currents inside conductor Induced currents oppose what created them (Lenz law)



Parabolic-elliptic equations

$$\partial_t(\sigma E) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E\right) = -\partial_t J \quad \text{in } \mathbb{R}^3 \times]0, T[$$

- parabolic inside conductor $\Omega = \operatorname{supp}(\sigma)$
- elliptic outside conductor

Scalar example: $(\sigma u)_t = u_{xx}$, $u(\cdot, 0) = 0$, $u_x(-2, \cdot) = u_x(2, \cdot) = 1$.







The direct problem

Unified variational formulation for the parabolic-elliptic eddy current problem



Standard approach

$$\partial_t(\sigma E) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E\right) = -\partial_t J \quad \text{in } \mathbb{R}^3 \times]0, T[$$

Standard approach: Decouple elliptic and parabolic part (e.g. Bossavit 1999, Acevedo/Meddahi/Rodriguez 2009)

Find $(E_{\mathbb{R}^3\setminus\Omega}, E_\Omega) \in H_{\mathbb{R}^3\setminus\Omega} \times H_\Omega$ s.t.

- E_{Ω} solves parabolic equation + init. cond.
- $E_{\mathbb{R}^3 \setminus \Omega}$ solves elliptic equation
- interface conditions are satisfied

Problem: Theory (solution spaces, coercivity constants, etc.) depends on $\Omega = \operatorname{supp} \sigma$ and on lower bounds of $\sigma|_{\Omega}$.



Unified approach?

Parabolic-elliptic eddy current equation

$$\partial_t(\sigma E) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E\right) = -\partial_t J \quad \text{in } \mathbb{R}^3 \times]0, T[$$

Inverse problem: Find σ (or $\Omega = \operatorname{supp} \sigma$) from measurements of E

requires unified solution theory

Test for unified theory: Can we linearize E w.r.t. σ ?

How does the solution of an elliptic equation change if the equation becomes a little bit parabolic?

(For scalar analogue: Frühauf/H./Scherzer 2007, H. 2007)



Rigorous formulation

Rigorous formulation: Let $\mu \in L^{\infty}_+$, $\sigma \in L^{\infty}$, $\sigma \ge 0$,

$$egin{aligned} &J_t\in L^2(0,\,T,\,W(\operatorname{curl})') & ext{ with } \operatorname{div} J_t=0\ &E_0\in L^2(\mathbb{R}^3)^3 & ext{ with } \operatorname{div}(\sigma E_0)=0. \end{aligned}$$

For $E \in L^2(0, T, W(curl))$ the eddy current equations

$$\partial_t(\sigma E) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E\right) = -J_t \quad \text{in } \mathbb{R}^3 \times]0, T[$$
$$\sqrt{\sigma}E(x,0) = \sqrt{\sigma(x)}E_0(x) \quad \text{in } \mathbb{R}^3$$

are well-defined and (if solvable) uniquely determine curl E, $\sqrt{\sigma E}$.



Natural variational formulation

Natural unified variational formulation ($E_0 = 0$ for simplicity):

Find $E \in L^2(0, T, W(\text{curl}))$ that solves

$$\int_0^T \int_{\mathbb{R}^3} \left(\sigma E \cdot \partial_t \Phi - \frac{1}{\mu} \operatorname{curl} E \cdot \operatorname{curl} \Phi \right) = \int_0^T \int_{\mathbb{R}^3} J_t \cdot \Phi.$$

for all smooth Φ with $\Phi(\cdot, T) = 0$.

- equivalent to eddy current equation
- not coercive, does not yield existence results



Gauged formulation

Gauged unified variational formulation ($E_0 = 0$ for simplicity)

Find divergence-free $E \in L^2(0, T, W^1(\mathbb{R}^3))$ that solves

$$\int_0^T \int_{\mathbb{R}^3} \left(\sigma E \cdot \partial_t \Phi - \frac{1}{\mu} \operatorname{curl} E \cdot \operatorname{curl} \Phi \right) = \int_0^T \int_{\mathbb{R}^3} J_t \cdot \Phi.$$

for all smooth divergence-free Φ with $\Phi(\cdot, T) = 0$.

- coercive, yields existence and continuity results
- not equivalent to eddy current equation ($\sigma \neq \text{const.} \rightsquigarrow \text{div } \sigma E \neq \sigma \text{ div } E$)
- does not determine true solution up to gauge (curl-free) field

Coercive unified formulation

How to obtain coercive + equivalent unified formulation?

 Ansatz E = A + ∇φ with divergence-free A. (almost the standard (A, φ)-formulation with Coulomb gauge)

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• Consider $\nabla \varphi = \nabla \varphi_A$ as function of A by solving div $\sigma \nabla \varphi_A = -\operatorname{div} \sigma A$.

($\rightsquigarrow \operatorname{div} \sigma E = 0$).

- Obtain coercive formulation for A (Lions-Lax-Milgram Theorem ~> Solvability and continuity results)
- ► A determines E (more precisely: curl E and √σE)



Unified variational formulation

Unified variational formulation (Arnold/H., SIAP, 2012)

Find divergence-free $A \in L^2(0, T, W^1(\mathbb{R}^3))$ that solves

$$\int_0^T \int_{\mathbb{R}^3} \left(\sigma(A + \nabla \varphi_A) \cdot \partial_t \Phi - \frac{1}{\mu} \operatorname{curl} A \cdot \operatorname{curl} \Phi \right) = \int_0^T \int_{\mathbb{R}^3} J_t \cdot \Phi.$$

for all smooth divergence-free Φ with $\Phi(\cdot, T) = 0$.

coercive, uniquely solvable

- $E := A + \nabla \varphi_A$ is one solution of the eddy current equation
- \rightsquigarrow curl *E*, $\sqrt{\sigma E}$ depend continuously on J_t (uniformly w.r.t. σ) (for all solutions of the eddy current equation)

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Asymptotic results

Unified variational formulation

- allows to rigorously linearize E w.r.t. σ around σ₀ = 0 (elliptic equation becoming a little bit parabolic in some region...)
- ► easily extends from \mathbb{R}^3 to bounded domain *O* (*O* simply conn. with Lipschitz-boundary, $\nu \wedge E|_{\partial O} = 0$)
- justifies parabolic regularization: If E_{ϵ} solves

$$\partial_t(\sigma_\epsilon E_\epsilon) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E_\epsilon\right) = -\partial_t J \quad \text{in } O \times]0, T[,$$

with $\sigma_\epsilon(x) = \max\{\sigma(x), \epsilon\}$ then
 $\sigma_\epsilon E_\epsilon \to \sigma E, \quad \operatorname{curl} E_\epsilon \to \operatorname{curl} E$

(Arnold/H., submitted to proceedings of IPDO 2013)

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Open problems

- Theory requires some regularity of Ω = supp σ and σ ∈ L[∞]₊(Ω) in order to determine φ from A.
- Solution theory for

$$\operatorname{div} \sigma \nabla \varphi = -\operatorname{div} \sigma A$$

for general $\sigma \in L^{\infty}$, $\sigma \geq 0$?

Elliptic regularization of the variational formulation

 (i.e., adding ε ∫₀^T ∫_{ℝ³} A · Φ dx)
 is justified, but relation to elliptic regularization of the PDE
 ∂_t(σE) + curl (¹/_μ curl E) + εE = -∂_tJ in ℝ³×]0, T[,

is not clear.





The inverse problem





Setup

Detecting conductors:

- Apply surface currents J on S (divergence-free, no electrostatic effects)
- Measure electric field E on S (tangential component, up to grad. fields)
- Measurement operator

$$\Lambda_{\sigma}: J_t \mapsto \gamma_{\tau} E := (\nu \wedge E|_{\mathcal{S}}) \wedge \nu$$

Locate $\Omega = \operatorname{supp} \sigma$ in

$$\partial_t(\sigma E) + \operatorname{curl}\left(\frac{1}{\mu}\operatorname{curl} E\right) = -J_t \quad \text{in } \mathbb{R}^3 \times]0, T[$$

(+ zero IC) from all possible surface currents and measured values.



Measurement operator

$$\begin{array}{ccc}
\nu & TL^2 := \{ u \in L^2(S)^3 \mid u \cdot \nu = 0 \} \\
S \subset \mathbb{R}^3_0 & TL^2_\diamond := \{ u \in TL^2 \mid \int_S u \cdot \nabla \psi = 0 \\
\forall \text{ smooth } \psi \}.
\end{array}$$

Measurement operator

$$\Lambda_{\sigma}: L^{2}(0, T, TL^{2}_{\diamond}) \rightarrow L^{2}(0, T, TL^{2'}_{\diamond}), \quad J_{t} \mapsto \gamma_{\tau} E,$$

where *E* solves eddy current eq. with $[\nu \times \text{curl } E]_S = J_t$ on *S*.

Remark

$${\it TL}^{2'}_{\diamond}\cong {\it TL}^2/{\it TL}^{2\perp}_{\diamond} \ \rightsquigarrow \ E$$
 not unique, but Λ_{σ} well-defined.



Sampling methods

Non-iterative shape detection methods:

- Linear Sampling Method (Colton/Kirsch 1996)
 - characterizes subset of scatterer by range test
 - allows fast numerical implementation
- Factorization Method (Kirsch 1998)
 - characterizes scatterer by range test
 - yields uniqueness under definiteness assumptions
 - allows fast numerical implementation
- Beyond LSM/FM?



Sampling ingredients

Ingredients for LSM and FM:

- ► Reference measurements: $\Lambda := \Lambda_{\sigma} \Lambda_0$, $\Lambda_0 : J_t \mapsto \gamma_{\tau} F$, F solves curl curl $F = -J_t$ in $\mathbb{R}^3 \times]0, T[$.
- ► Time-integration: Consider $I\Lambda$, with $I : E(\cdot, \cdot) \mapsto \int_0^T E(\cdot, t) dt$
- Singular test functions

$${\mathcal G}_{z,d}(x):=\operatorname{\mathsf{curl}} rac{d}{4\pi |x-z|},\qquad x\in {\mathbb R}^3\setminus\{z\}$$



LSM and FM

Arnold/H. (submitted): For every z below S, $z \notin \Omega$ and direction $d \in \mathbb{R}^3$.

Theorem (LSM)

$$\gamma_{\tau} \mathcal{G}_{z,d} \in \mathcal{R}(I\Lambda) \quad \Rightarrow \quad z \in \Omega$$

Theorem (FM) If, additionally, $\sup \mu|_{\Omega} < 1$ (diamagnetic scatterer) $\gamma_{\tau} G_{z,d} \in \mathcal{R}(I(\Lambda + \Lambda')^{1/2}) \quad \Leftrightarrow \quad z \in \Omega$



Beyond LSM/FM?

- Beyond LSM/FM?: Monotony methods
- ► For EIT: Λ_{σ} NtD-operator for conductivity $\sigma = 1 + \chi_D$ D = Union of all balls B where $\Lambda_{1+\chi_B} \leq \Lambda_{\sigma}$ (H./Ullrich) (under the assumptions of the FM)
- stable test criterion (no infinity tests)
- allows fast numerical implementation
- allows extensions to indefinite cases



Conclusions

Inverse transient eddy current problems

- require unified parabolic-elliptic theory
- can be approached by sampling methods (LSM/FM)

Open problems

Solution theory for

$$\operatorname{div} \sigma \nabla \varphi = -\operatorname{div} \sigma A$$

for general $\sigma \in L^{\infty}$, $\sigma \geq 0$?

Monotony based methods beyond EIT? Monotony for parabolic-elliptic problems?